

--3. (amended) Device (10) according to claim 1, characterized in that the axial displacement means (58) comprise a linear actuator (58) which is capable of axially displacing the load sensor (26) and its sensitive member (52).--

--4. (amended) Device (10) according to claim 1, characterized in that it comprises a load transmitter (52) which is inserted between the closure element (38) and the load sensor (26) which is fixed, and in that the displacement of the load transmitter (52), which is axial with respect to the load sensor (26), is controlled by a linear actuator (58).--

--5. (amended) Device (10) according to claim 3, characterized in that the linear actuator (58) comprises an electric motor (62) of the stepper-motor type.--

--6. (amended) Device (10) according to claim 1, characterized in that the closure element (38) is made in a single part with the associated rigid wall (34).--

--7. (amended) Device (10) according to claim 1, characterized in that the closure element (38) is moulded with the associated rigid wall (34).--

--8. (amended) Device (10) according to claim 1, characterized in that it comprises a control system which controls the axial displacement means (58) so that an initial calibration operation, which consists in choosing the axial position of the sensitive member (52), respectively of the

measurement section (16), with respect to the external face (42) of the closure element (38), respectively with respect to the axial end of the sensitive member (52), is carried out when the closure element (38) is in its rest state, this rest state corresponding to the absence of a pressure gradient between its external face (42) and its internal face (40).--

--9. (amended) Device (10) according to claim 8, characterized in that the control system controls the axial displacement means (58) so that, during the initial calibration operation, the axial displacement of the sensitive member (52) towards the external face (42) of the closure element (38), respectively the axial displacement of the measurement section (16) towards the axial end of the sensitive member (52), is provoked until to obtain an initial pretensioning force (F_0) which is high enough so that the pressure measurement device (10) works in a linear region of the axial displacement means (58) where axial play has no effect on the pressure measurements.--

--10. (amended) Device (10) according to claim 1, characterized in that it comprises a control system which controls the axial displacement means (58) so that the response of the closure element (38) to a pretensioning force (F_0) can be analysed as a function of an axial displacement of the sensitive member (52), respectively of the measurement section (16).--

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--11. (amended) Device (10) according to claim 10, characterized in that the analysis of the response of the closure element (38) is aimed to determine an optimum pretensioning force (F0) for measurements of blood pressure greater than the ambient air pressure and for measurements of blood pressure less than the ambient air pressure.--

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--13. (amended) Process according to claim 12, characterized in that the initial adjustment phase comprises an initial calibration operation, and that, during the initial calibration operation, the sensitive member (52), respectively the measurement section (16), is axially moved towards the external face (42) of the associated closure element (38), respectively towards the axial end of the associated sensitive member (52), up to a given axial position of reference in which the sensitive member (52) is in contact with the external face (42) of the closure element (38), with a view to establish a correlation between a given pretensioning force (F0) and the rest state of the closure element (38), this rest state corresponding to an absence of a pressure gradient between its external face (42) and its internal face (40).--

--14. (amended) Process according to claim 13, characterized in that, during the initial calibration operation, the sensitive member (52), respectively the measurement section (16), is axially moved towards the external face (42) of the closure element (38), respectively towards the axial end of the sensitive member (52), until the sensitive member

(52) applies an initial pretensioning force (F0) which is high enough so that the pressure measurement device (10) works in a linear region of the axial displacement means (58) where axial play has no effect on the pressure measurements.--

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--15. (amended) Process according to claim 12, characterized in that the initial adjustment phase comprises an analysis phase, and that the analysis phase consists in analysing the response of the closure element (38) to a pretensioning force (F0) varying as a function of an axial displacement of the sensitive member (52), respectively of the measurement section (16).--

--16. (amended) Process according to claim 15, characterized in that the analysis phase is used for the purpose of identifying a fault in the structure of the closure element (38).

--17. (amended) Process according to claim 15, characterized in that the analysis phase is used for the purpose of determining an optimum pretensioning force (F0) for measurements of blood pressure greater than the ambient air pressure and for measurements of blood pressure less than the ambient air pressure.--

R E M A R K S

Attached hereto is a marked-up version of the changes made to the claims by the current amendment. The